

DESCRIPTION

BATTERY CONNECTION DETECTION CIRCUIT

5 TECHNICAL FIELD

The present invention relates to a battery connection detection circuit of a charging device for charging a secondary battery in connection, and particularly, to a battery connection detection circuit
10 for detecting whether the secondary battery is in reliable connection with the charging device, whether the secondary battery in connection with the charging device has a low internal impedance, and whether the secondary battery is in good condition and is able to be charged.

15

BACKGROUND ART

In order to detect connection conditions of a secondary battery connected to a charging device, such as a lithium-ion battery, usually a thermistor installed in
20 the secondary battery can be used to detect the temperature of the secondary battery being charged, or a built-in resistor can be used to detect the connection conditions of the secondary battery. Specifically, a current is directed to flow through the thermistor or the
25 resistor, and a voltage occurring between two ends of

them is measured to detect the battery connection conditions. Alternatively, as a well known method, a current is directed to flow through the secondary battery connected to the charging device, and a voltage between
5 two battery connection terminals of the charging device can be measured to determine whether the battery is reliably connected.

In the former method, when the secondary battery is connected to the charging device, even if the
10 terminals of the thermistor or the resistor and the charging device are reliably connected, it cannot be guaranteed that the electrode of the secondary battery and the charging device are reliably connected. In other words, even when the charging device charges the
15 secondary battery assuming the secondary battery is reliably connected, sometimes, because the battery connection terminal actually is not in contact with the electrode of the battery, the secondary battery is actually not charged. Similarly, even when the electrode
20 of the battery is connected to the charging device, if the thermistor or the resistor is not in good connection condition, temperature control cannot be carried out appropriately in the course of charging, insufficient charging happens, and the secondary battery may
25 experience problems.

FIG. 7 is a block diagram showing an internal configuration of a charging device 100 of the related art, presenting a method of confirming the voltage on a secondary battery BAT mounted on the charging device 100.

5 As illustrated in FIG. 7, a charging control circuit 101, which functions as a detection circuit for detecting whether the secondary battery BAT is reliably connected, includes a preliminary charging constant-current circuit 102 for supplying a predetermined current
10 to the secondary battery BAT, a diode Da for preventing a reverse current, a battery pack voltage detection circuit 103 for detecting the voltage on a battery connection terminal Ta of the charging device 100, a current detection circuit 104, and a charging FET control circuit
15 105. A resistance component r corresponds to the sum of the internal resistance of the secondary battery BAT and the contact resistance between an electrode of the secondary battery BAT and the battery connection terminal Ta of the charging device 100.

20 When the secondary battery BAT is reliably connected, the impedance of the resistance component r is small, and it is thought that the change of the voltage caused by the resistance component r is negligible, hence, the voltage on a battery connection terminal Ta equals
25 the voltage on the secondary battery BAT. However, the

impedance of the resistance component r increases if the secondary battery BAT is not appropriately connected, or even though the secondary battery BAT is appropriately connected, the electrode of the secondary battery BAT and the battery connection terminal Ta of the charging device 100 are not in good connection conditions, resulting in a large contact resistance between them, or the secondary battery BAT is not in good connection conditions, and has a large internal resistance.

10 In these cases, even when a small current is supplied to the secondary battery BAT, the voltage on the battery connection terminal Ta of the charging device 100 increases up to the voltage on an input terminal (IN) connected to an AC adapter. From these facts, the battery
15 pack voltage detection circuit 103 detects that the voltage on the secondary battery BAT reaches an unspecified value, and with the detection results, it is possible to reliably connect the battery.

 For example, Japanese Laid Open Patent
20 Application No. 5-219656 discloses a battery charger which has a charging mode and an adapter mode, and when bad connection conditions or other anomalies are detected, the battery charger shows an alarm and stop output.

 The charging device of the related art,
25 however, is supplied with a DC current from an AC adapter,

which works as a power supply. Due to this, high frequency noise superposed on the AC line is also superposed on the power supply voltage Vdd. Namely, the high frequency noise also influences the battery connection terminal Ta, and sometimes, the high frequency noise may also be superposed on the voltage on the battery connection terminal Ta. When the voltage superposed with the high frequency noise reaches an unspecified value for the secondary battery BAT, a determination is made that bad connection conditions occur. In addition, when the voltage of the AC line decreases depending on the load of the charging device 100, the voltage on the battery connection terminal Ta does not reach a battery pack unspecified value inside the charging device, and this cannot be determined as bad connection conditions.

DISCLOSURE OF THE INVENTION

It is a general object of the present invention to solve one or more of the problems of the related art.

A specific object of the present invention is to provide a battery connection detection circuit that is able to correctly determine an operation condition of a secondary battery and a connection condition between the

secondary battery and a charging device even when high frequency noise is superposed on a power supply of the charging device, and even when an output voltage of the power supply decreases.

5 According to the present invention, there is provided a battery connection detection circuit for detecting whether a secondary battery is operable and whether the secondary battery is reliably connected to a charging device, comprising: a current supplying circuit
10 configured to supply a current to the secondary battery; a constant voltage circuit configured to control the current from the current supplying circuit so that a voltage on a connection terminal T1 for connecting the secondary battery is constant; a constant current circuit
15 configured to control the current from the current supplying circuit so that the current supplied to the secondary battery is constant; and a determination circuit configured to determine operation states of the constant voltage circuit and the constant current circuit,
20 said determination circuit determining whether the secondary battery is operable and whether the secondary battery is reliably connected to the charging device according to the operation states of the constant voltage circuit and the constant current circuit.

25 In an embodiment, the determination circuit

determines an operation state of a load circuit that receives power supply from the secondary battery; and when it is detected that the load circuit does not consume a current, the determination circuit determines
5 whether the secondary battery is operable and whether the secondary battery is reliably connected to the charging device according to the operation states of the constant voltage circuit and the constant current circuit.

In an embodiment, when it is determined that
10 the voltage on the connection terminal T1 is lower than a predetermined value from the operation state of the constant current circuit, or the current flowing through the secondary battery is higher than a predetermined value from the operation state of the constant current
15 circuit, the determination circuit determines the secondary battery is operable and the secondary battery is reliably connected to the connection terminal T1.

In an embodiment, the current supplying circuit includes a current control transistor that
20 controls the current supplied to the secondary battery according to a control signal input to a control electrode thereof; the constant voltage circuit includes a voltage detection circuit that detects the voltage on the connection terminal T1 and outputs a voltage Vd1
25 proportional to the detected voltage, a first calculation.

amplification circuit into which the output voltage V_{d1} from the voltage detection circuit and a first reference voltage V_{s1} are input, and a first control transistor whose operation is controlled according to an output signal CV from the first calculation amplification circuit; the constant current circuit includes a current detection circuit that converts the current supplied by the current supplying circuit into a voltage and outputs the voltage, a second calculation amplification circuit into which the output voltage from the current detection circuit and a second reference voltage V_{s2} are input, and a second control transistor whose operation is controlled according to an output signal CC from the second calculation amplification circuit; and the current control transistor controls the current supplied to the secondary battery according to operations of the first control transistor and the second control transistor.

Alternatively, as an embodiment, the current supplying circuit includes a current control transistor that controls the current supplied to the secondary battery according to a control signal input to a control electrode thereof; the constant voltage circuit includes a voltage detection circuit that detects the voltage on the connection terminal T1 and outputs a voltage V_{d1} proportional to the detected voltage, a switching circuit

that exclusively selects one of a plurality of input reference voltages V_{r1} to V_{rn} according to an input control signal S_{c1} , and outputs the selected reference voltage as a first reference voltage V_{s1} , a first
5 calculation amplification circuit into which the output voltage V_{d1} from the voltage detection circuit and the first reference voltage V_{s1} are input, and a first control transistor whose operation is controlled according to an output signal CV from the first
10 calculation amplification circuit; the constant current circuit includes a current detection circuit that converts the current supplied by the current supplying circuit into a voltage and outputs the voltage, a second calculation amplification circuit into which the output
15 voltage from the current detection circuit and a second predetermined reference voltage V_{s2} are input, and a second control transistor whose operation is controlled according to an output signal CC from the second calculation amplification circuit; and the current
20 control transistor controls the current supplied to the secondary battery according to operations of the first control transistor and the second control transistor.

In an embodiment, the operation state of the constant voltage circuit corresponds to a state of the
25 output signal CV from the first calculation amplification

circuit; and the operation state of the constant current circuit corresponds to a state of the output signal CC from the second calculation amplification circuit.

In an embodiment, the current control
5 transistor includes a MOS transistor, or a bipolar transistor.

In an embodiment, the determination circuit determines the secondary battery is operable and the secondary battery is reliably connected to the connection
10 terminal T1, when the output signal CV from the first calculation amplification circuit indicates that the output voltage Vd1 from the voltage detection circuit is lower than the first reference voltage Vs1, or when the output signal CC from the second calculation
15 amplification circuit indicates that the output voltage from the current detection circuit is higher than or equal to the second reference voltage Vs2.

In an embodiment, the current supplying circuit, the constant voltage circuit, the constant
20 current circuit, and the determination circuit are integrated in one Integrated Circuit (IC).

In an embodiment, the current supplying circuit, the constant voltage circuit, the constant current circuit, the determination circuit, and the load
25 circuit are integrated in one Integrated Circuit (IC).

According to the battery connection detection circuit of the present invention, two factors, namely, the voltage on the connection terminal T1 and the current flowing through the secondary battery are used in order
5 to determine whether the secondary battery is operable and whether the secondary battery is reliably connected to the connection terminal T1. In doing so, it is possible to correctly determine the operation condition of the secondary battery and the connection condition
10 between the secondary battery and the charging device even when high frequency noise is superposed on the power supply of the charging device, and even when the output voltage of the power supply decreases.

In addition, because when the load circuit
15 does not consume a current, the determination circuit determines whether the secondary battery is operable and whether the secondary battery is reliably connected to the charging device, it is possible to further improve reliability of the determination.

20 Further, because a bipolar transistor is used in the current control transistor in the current supplying circuit which supplies a current to the secondary battery, the high frequency noise superposed on the power supply voltage can hardly be transmitted to the
25 connection terminal T1, hence, it is possible to further

improve reliability of the determination.

These and other objects, features, and advantages of the present invention will become more apparent from the following detailed description of preferred embodiments given with reference to the accompanying drawings

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a circuit diagram showing an example of a configuration of a battery connection detection circuit according to a first embodiment of the present invention;

FIG. 2 shows dependence of the output signal CV from the first calculation amplification circuit AMP1 and the output signal CC from the second calculation amplification circuit AMP2 on the impedance of the resistance component r ;

FIG. 3 is a circuit diagram showing another example of a configuration of the battery connection detection circuit according to the first embodiment of the present invention;

FIG. 4 is a circuit diagram showing an example of a configuration of a battery connection detection circuit according to a second embodiment of the present invention;

FIG. 5 is a circuit diagram showing an example of a configuration of a battery connection detection circuit according to a third embodiment of the present invention;

5 FIG. 6 is a circuit diagram showing another example of the battery connection detection circuit according to the third embodiment of the present invention; and

FIG. 7 is a block diagram showing an internal
10 configuration of a charging device of the related art.

BEST MODE FOR CARRYING OUT THE INVENTION

Below, preferred embodiments of the present invention are explained with reference to the
15 accompanying drawings.

First Embodiment

FIG. 1 is a circuit diagram showing an example of a configuration of a battery connection detection
20 circuit 1 according to a first embodiment of the present invention.

The battery connection detection circuit 1 shown in FIG. 1 is installed in a charging device for a secondary battery.

25 As illustrated in FIG. 1, the battery

connection detection circuit 1 includes a PMOS transistor M1 for supplying a current to a secondary battery BAT, a constant resistance R1 for detecting the current flowing through the PMOS transistor M1, constant resistances R2 and R3 for detecting the voltage Vt1 on a battery connection terminal T1 of the charging device, a resistance R4 functioning as a pull-up resistance, a first reference voltage generation circuit 2 that generates and outputs a first reference voltage Vs1, a first calculation amplification circuit AMP1, a second calculation amplification circuit AMP2, and NMOS transistors M2, M3.

The battery connection detection circuit 1 includes a current detection circuit 3 that converts a voltage drop on the resistance R1 to a voltage relative to a grounding voltage reference, and outputs the voltage, a second reference voltage generation circuit 4 that generates and outputs a second reference voltage Vs2, and a determination circuit 5 that determines whether the secondary battery BAT is operable and whether the secondary battery BAT is reliably connected to the charging device.

Here, the PMOS transistor M1 and the resistance R4 constitute the current supplying circuit in the claims, the first calculation amplification circuit

AMP1, the first reference voltage generation circuit 2,
the NMOS transistor M2, and resistances R2 and R3
constitute the constant voltage circuit in the claims. In
addition, the PMOS transistor M1 corresponds to the
5 current control transistor, and the resistances R2 and R3
correspond to the voltage detection circuit in the claims.
Further, the current detection circuit 3, the second
calculation amplification circuit AMP2, the NMOS
transistor M3, and the resistance R1 constitute the
10 constant current circuit in the claims, the NMOS
transistor M2 corresponds to the first control transistor
in the claims, and the NMOS transistor M3 corresponds to
the second control transistor in the claims.

In FIG. 1, a power supply voltage Vdd is input
15 from an AC adapter 10 to an input terminal IN. The PMOS
transistor M1 is connected in series between the input
terminal IN and the battery connection terminal T1, and a
resistance component r and the secondary BAT are
connected in series between the battery connection
20 terminal T1 and the ground. The resistance component r
corresponds to the sum of the internal resistance of the
secondary battery BAT and the contact resistance between
an electrode of the secondary battery BAT and the battery
connection terminal T1. The NMOS transistors M2, M3 are
25 connected in series between the gate of the PMOS

transistor M1 and the ground, and the resistance R4 is connected between the input terminal IN and the gate of the PMOS transistor M1.

The gate of the NMOS transistor M2 is
5 connected to an output terminal of the first calculation amplification circuit AMP1, and the first reference voltage V_{s1} is input to a non-inverted input terminal of the first calculation amplification circuit AMP1. The resistances R2, R3 are connected in series between the
10 battery connection terminal T1 and the ground, and the connecting point of the resistances R2, R3 is connected to the non-inverted input terminal of the first calculation amplification circuit AMP1.

In addition, the current detection circuit 3
15 is driven by the power supply voltage V_{dd} and the ground voltage, converts the voltage at the connecting point between the resistance R1 and the PMOS transistor M1 to a voltage relative to the grounding voltage, and outputs the voltage to an inverted input terminal of the second
20 calculation amplification circuit AMP2. The output signal CV from the first calculation amplification circuit AMP1 and the output signal CC from the second calculation amplification circuit AMP2 are transmitted to the determination circuit 5.

25 FIG. 2 shows dependence of the output signal

CV from the first calculation amplification circuit AMP1 and the output signal CC from the second calculation amplification circuit AMP2 on the impedance of the resistance component r . Below, operations of the battery connection detection circuit 1 with the above configuration are exemplified with reference to FIG. 2.

Below, it is assumed that an operable secondary battery BAT, which has small internal resistance, is installed in the charging device, and the contact resistance between the electrode of the secondary battery BAT and the battery connection terminal T1 is small, that is, the impedance of the resistance component r is small.

Under these conditions, even when a current is supplied to the secondary battery BAT through the PMOS transistor M1, the voltage V_{t1} on the battery connection terminal T1 is small, and the voltage input to the inverted input terminal of the first calculation amplification circuit AMP1 is lower than the first reference voltage V_{s1} . Due to this, the output signal CV from the first calculation amplification circuit AMP1 is at a high level, and the NMOS transistor M2 is switched on.

The current flowing through the PMOS transistor M1 is converted to a voltage at the resistance

R1, and this voltage is converted to a voltage relative to the grounding voltage by the current detection circuit 3, and is input to the inverted input terminal of the second calculation amplification circuit AMP2.

5 The second reference voltage Vs2 is input to a non-inverted input terminal of the second calculation amplification circuit AMP2, and the output signal CC from the second calculation amplification circuit AMP2 controls operations of the NMOS transistor M3 so that the
10 output voltage of the current detection circuit 3 is equal to the second reference voltage Vs2. As a result, the current flowing through the PMOS transistor M1 is controlled to be a constant current. In other words, as illustrated in FIG. 2, when the impedance of the
15 resistance component r is small, the output signal CV from the first calculation amplification circuit AMP1 is at the high level, and the output signal CC from the second calculation amplification circuit AMP2 is at a low level near the threshold voltage of the NMOS transistor
20 M3.

Next, it is assumed that a defective secondary battery BAT, which has large internal resistance, is installed in the charging device, and the contact resistance between the electrode of the secondary battery
25 BAT and the battery connection terminal T1 is large, that

is, the impedance of the resistance component r is small.

Under these conditions, even when a small current is supplied to the secondary battery BAT through the PMOS transistor M1, the voltage V_{t1} on the battery connection terminal T1 is large. When the voltage V_{t1} on the battery connection terminal T1 reaches the first reference voltage V_{s1} , the level of the output signal CV from the first calculation amplification circuit AMP1 decreases, and the voltage V_{t1} on the battery connection terminal T1 is controlled so that the voltage V_{d1} at the connecting point between the resistances R_2 , R_3 becomes equal to the first reference voltage V_{s1} .

As a result, the current flowing through the PMOS transistor M1 decreases compared to the case when the impedance of the resistance component r is small, the output voltage of the current detection circuit 3 is lower than the second reference voltage V_{s2} , and the output signal CC from the second calculation amplification circuit AMP2 is at the high level.

In other words, as illustrated in FIG. 2, when the impedance of the resistance component r is large, the output signal CC from the second calculation amplification circuit AMP2 is at the high level, and the output signal CV from the first calculation amplification circuit AMP1 is at a low level near the threshold voltage

of the NMOS transistor M2.

If the limit of the impedance of the resistance component r is set to be a normalized value r_1 as indicated in FIG. 2, it is clear that the condition
5 for the secondary battery BAT to have small internal resistance, and the electrode of the secondary battery BAT to be reliably connected to the battery connection terminal T1 is that the impedance is on the left side of the normalized value r_1 , that is, the impedance is less
10 than the normalized value r_1 .

In other words, a determination condition may be set such that the determination circuit 5 determines the battery connection condition is good, when the output signal CV from the first calculation amplification
15 circuit AMP1 is at the high level, or when the output signal CC from the second calculation amplification circuit AMP2 is at the high level, or when both the output signal CV from the first calculation amplification circuit AMP1 and the output signal CC from the second
20 calculation amplification circuit AMP2 are at the high level.

In this way, not only the voltage V_{t1} on the battery connection terminal T1, but also the current supplied to the secondary battery BAT are monitored,
25 thereby, it is possible to perform battery connection

detection without influence from the power supply voltage Vdd.

For example, the first reference voltage generation circuit 2, the current detection circuit 3, the second reference voltage generation circuit 4, the determination circuit 5, the first calculation amplification circuit AMP1, the second calculation amplification circuit AMP2, the PMOS transistor M1, the NMOS transistors M2, M3, and the resistances R1 to R4 can be integrated into one Integrated Circuit (IC).

In addition, instead of the PMOS transistor M1 in FIG. 1, a bipolar transistor may be used.

FIG. 3 is a circuit diagram showing another example of a configuration of the battery connection detection circuit 1 according to the first embodiment of the present invention.

When a bipolar transistor is used instead of the PMOS transistor M1, the battery connection detection circuit 1 has a circuit configuration as shown in FIG. 3. In FIG. 3, a pnp transistor Q1 functions as the current supplying circuit and as the current control transistor in the claims.

By replacing the PMOS transistor M1 with the pnp transistor Q1, the resistance R4 in FIG. 4 can be omitted, and the impedance of the drain of the NMOS

transistor M2 is lowered, and the high frequency noise superposed on the power supply voltage Vdd can hardly be transmitted to the connection terminal T1, and hence, it is possible to further improve reliability of battery connection detection.

Similarly, in this example, the first reference voltage generation circuit 2, the current detection circuit 3, the second reference voltage generation circuit 4, the determination circuit 5, the first calculation amplification circuit AMP1, the second calculation amplification circuit AMP2, the pnp transistor Q1, the NMOS transistors M2, M3, and the resistances R1 to R3 can be integrated into one Integrated Circuit (IC).

According to the present embodiment, because both the voltage Vt1 on the battery connection terminal T1 and the current supplied to the secondary battery BAT are monitored, it is possible to correctly determine the operation condition of the secondary battery BAT and the connection condition between the secondary battery BAT and the charging device even when high frequency noise is superposed on the power supply voltage Vdd, and when the power supply voltage decreases.

FIG. 4 is a circuit diagram showing an example of a configuration of a battery connection detection circuit 1a according to a second embodiment of the present invention.

5 In the previous embodiment, the first reference voltage V_{s1} input to the non-inverted input terminal of the first calculation amplification circuit AMP1 is one voltage signal.

 Meanwhile, in the present embodiment, one of
10 plural reference voltage signals V_{r1} to V_{rn} is selected and used as the first reference voltage V_{s1} .

 In FIG. 4, the same reference numbers are used for the same elements as those in the previous embodiment, and only differences with the first embodiment are
15 described in detail with overlapping descriptions being omitted.

 The battery connection detection circuit 1a in FIG. 4 differs from the battery connection detection circuit 1 in FIG. 1 in that the first reference voltage
20 generation circuit generates plural reference voltages V_{r1} to V_{rn} (n is an integer greater than 1), and a switching circuit 21 is provided to exclusively select one of the reference voltages V_{r1} to V_{rn} according to an input control signal S_{c1} , and outputs the selected
25 reference voltage to the non-inverted input terminal of

the first calculation amplification circuit AMP1 as the first reference voltage Vs1. Accordingly, the battery connection detection circuit 1 and the first reference voltage generation circuit 2 in FIG. 1 are indicated as the battery connection detection circuit 1a and the first reference voltage generation circuit 2a, respectively.

In FIG. 4, the battery connection detection circuit 1a includes a PMOS transistor M1, resistances R1 to R4, the first reference voltage generation circuit 2a that generates and outputs reference voltages Vr1 to Vrn, and the switching circuit 21. Further, the battery connection detection circuit 1a includes the first calculation amplification circuit AMP1, the second calculation amplification circuit AMP2, the NMOS transistors M2, M3, the current detection circuit 3, the second reference voltage generation circuit 4, and the determination circuit 5.

Here, the first calculation amplification circuit AMP1, the first reference voltage generation circuit 2a, the switching circuit 21, the NMOS transistor M2, and resistances R2 and R3 constitute the constant voltage circuit in the claims.

The reference voltages Vr1 to Vrn from the first reference voltage generation circuit 2a are input to the switching circuit 21, and an external control

signal Scl is input to the switching circuit 21.

According to the control signal Scl, the switching circuit 21 exclusively selects one of the reference voltages Vrl to Vrn, and outputs the selected
5 reference voltage to the non-inverted input terminal of the first calculation amplification circuit AMP1 as the first reference voltage Vs1.

For example, if $n = 2$, from the signal CV with the reference voltage Vrl as the first reference voltage
10 Vs1, and the signal CV with the reference voltage Vr2 as the first reference voltage Vs1, the determination circuit 5 can determine whether the secondary battery BAT is reliably connected to the connection terminal T1.

Further, if $n > 2$, from the signals CV
15 respectively corresponding to the reference voltages Vrl to Vrn, the determination circuit 5 can determine the value range of the resistance component r , and control charging of the secondary battery BAT according to the resistance component r .

20 Similarly, the first reference voltage generation circuit 2a, the current detection circuit 3, the second reference voltage generation circuit 4, the determination circuit 5, the switching circuit 21, the first calculation amplification circuit AMP1, the second
25 calculation amplification circuit AMP2, the PMOS

transistor M1, the NMOS transistors M2, M3, and the resistances R1 to R4 can be integrated into one Integrated Circuit (IC).

According to the present embodiment, the same effects as the first embodiment are obtainable. In addition, by changing the first reference voltage V_{s1} , it is possible to determine the impedance of the resistance component r , thereby further improving reliability when determining the connection condition of the secondary battery BAT. In addition, because the range of the impedance of the resistance component r can be determined, it is possible to control charging of the secondary battery BAT according to the resistance component r .

15 Third Embodiment

FIG. 5 is a circuit diagram showing an example of a configuration of a battery connection detection circuit 1b according to a third embodiment of the present invention.

20 In the present embodiment, a load circuit is connected to the secondary battery BAT, and it is configured so that the connection condition of the secondary battery BAT is detected when the load circuit does not produce current consumption.

25 In FIG. 5, the same reference numbers are used

for the same elements as those in the previous embodiments, and only differences with the previous embodiments are described in detail with overlapping descriptions being omitted.

5 The battery connection detection circuit 1b in FIG. 5 differs from the battery connection detection circuit 1 in FIG. 1 in that an external load circuit 30 is provided, which includes a constant voltage circuit 31, a load circuit 32, and a load current detection circuit
10 33.

 The constant voltage circuit 31, with the voltage V_{t1} on the battery connection terminal T1 as a power supply, generates a constant voltage V1. The load circuit 32 is driven to operate by the constant voltage
15 V1. The load current detection circuit 33 detects the current through the load circuit 32.

 The load current detection circuit 33 outputs a state signal S1 to the determination circuit 5, which indicates current consumption state of the load circuit
20 32, and the determination circuit 5 detects the connection condition of the secondary battery BAT when the load circuit 32 does not produce current consumption.

 In FIG. 5, the battery connection detection circuit 1 and the determination circuit 5 in FIG. 1 are
25 indicated as the battery connection detection circuit 1b

and the determination circuit 5b, respectively.

In FIG. 5, the constant voltage circuit 31 is driven by the voltage V_{t1} at the battery connection terminal T1 to generate the constant voltage V_1 , and
5 outputs the constant voltage V_1 to the load circuit 32. The load circuit 32 is driven to operate by the constant voltage V_1 . The load current detection circuit 33 detects the current supplied from the constant voltage circuit 31 to the load circuit 32, and outputs a state signal S1 to
10 the determination circuit 5 when the load circuit 32 does not produce current consumption. In this situation, the current consumption of the constant voltage circuit 31 is very small and is negligible.

When the state signal S1 is input to the
15 determination circuit 5b from the load current detection circuit 33, as described in the first embodiment, the determination circuit 5b starts operations of detecting the connection condition of the secondary battery BAT based on the output signal CV from the first calculation
20 amplification circuit AMP1 and the output signal CC from the second calculation amplification circuit AMP2. If the state signal S1 is not input, the determination circuit 5b stops detection of connection condition of the secondary battery BAT.

25 For example, the first reference voltage

generation circuit 2, the current detection circuit 3,
the second reference voltage generation circuit 4, the
determination circuit 5b, the first calculation
amplification circuit AMP1, the second calculation
5 amplification circuit AMP2, the PMOS transistor M1, the
NMOS transistors M2, M3, and the resistances R1 to R4 can
be integrated into one Integrated Circuit (IC).
Furthermore, the external load circuit 30 may also be
integrated into the IC.

10 FIG. 6 is a circuit diagram showing another
example of the battery connection detection circuit 1b
according to the third embodiment of the present
invention, having a configuration in correspondence to
the battery connection detection circuit in FIG. 4. In
15 FIG. 6, the same reference numbers are used for the same
elements as those in the previous embodiments, and
overlapping descriptions are omitted.

 When the state signal S1 is input to the
determination circuit 5b from the load current detection
20 circuit 33, as described in the second embodiment, the
determination circuit 5b starts operations of detecting
the connection condition of the secondary battery BAT
based on the output signal CV from the first calculation
amplification circuit AMP1 and the output signal CC from
25 the second calculation amplification circuit AMP2. If the

state signal S1 is not input to the determination circuit 5b, the determination circuit 5b stops detection of connection condition of the secondary battery BAT.

For example, the first reference voltage generation circuit 2a, the current detection circuit 3, the second reference voltage generation circuit 4, the determination circuit 5b, the switching circuit 21, the first calculation amplification circuit AMP1, the second calculation amplification circuit AMP2, the PMOS transistor M1, the NMOS transistors M2, M3, and the resistances R1 to R4 can be integrated into one Integrated Circuit (IC). Furthermore, the external load circuit 30 may also be integrated into the IC.

When the load circuit 32 does not produce current consumption, the impedance at the battery connection terminal T1 substantially corresponds only to the impedance of the resistance component r. Due to this, in the present embodiment, it is configured so that the determination circuit 5b starts operations of detecting the connection condition of the secondary battery BAT when the load circuit 32 does not produce current consumption.

As a result, the same effects as those of the first embodiment are obtainable. In addition, it is possible to more accurately perform connection condition

detection of the secondary battery BAT.

While the present invention is above described with reference to specific embodiments chosen for purpose of illustration, it should be apparent that the invention is not limited to these embodiments, but numerous modifications could be made thereto by those skilled in the art without departing from the basic concept and scope of the invention.

According to the present invention, both the voltage on the connection terminal and the current flowing through the secondary battery are used for detecting the operation conditions of the secondary battery and the connection conditions between the secondary battery and the charging device, it is possible to provide a battery connection detection circuit that is able to correctly determine the operation condition of the secondary battery and the connection condition between the secondary battery and the charging device even when high frequency noise is superposed on the power supply of the charging device, and even when the output voltage of the power supply decreases.

In addition, the operation conditions of the secondary battery and the connection conditions between the secondary battery and the charging device are detected when the load circuit does not consume a current,

thus, it is possible to further improve reliability of the determination.

Further, because a bipolar transistor is used in the current control transistor in the current
5 supplying circuit which supplies a current to the secondary battery, the high frequency noise superposed on the power supply voltage can hardly be transmitted to the connection terminal T1, hence, it is possible to further improve reliability of the determination.

10 This patent application is based on Japanese Priority Patent Application No. 2003-091307 filed on March 28, 2003, the entire contents of which are hereby incorporated by reference.